

### STATE SPACE REPRESENTATION:

$$\ddot{y} + 2\dot{y} + 3y = u$$

introduce new variables.

$$x_1 = y$$

$$x_2 = \dot{y}$$

$$\therefore \dot{x}_1 = \dot{y} = x_2, \quad \dot{x}_2 = \ddot{y} = -3y - 2\dot{y} + u = -3x_1 - 2x_2 + u$$

$$\ddot{y} = -3y - 2\dot{y} + u = -3x_1 - 2x_2 + u$$

$$\dot{x}_1 = x_2$$

$$\dot{x}_2 = -3x_1 - 2x_2 + u$$

$x_1, x_2$  are state variables.

$$\underbrace{\begin{bmatrix} \dot{x}_1 \\ \dot{x}_2 \end{bmatrix}}_{\dot{x}} = \underbrace{\begin{bmatrix} 0 & 1 \\ -3 & -2 \end{bmatrix}}_A \underbrace{\begin{bmatrix} x_1 \\ x_2 \end{bmatrix}}_x + \underbrace{\begin{bmatrix} 0 \\ 1 \end{bmatrix}}_B u$$

$$\dot{x} = Ax + Bu$$

note:  $x$  is known as the state vector.

$$y = Cx + Du$$

note: in most practical systems,  $D$  matrix is zero.

note: the eigen values of the  $A$  matrix are the poles of the original system.

Ex: calculating eigen values of  $A$ .

$d_1, d_2$  are the eigen values of  $A$ .

$$\det(dI - A) = 0$$

$$dI - A = \begin{bmatrix} d & 0 \\ 0 & d \end{bmatrix} - \begin{bmatrix} 0 & 1 \\ -3 & -2 \end{bmatrix} = \begin{bmatrix} d & -1 \\ 3 & d+2 \end{bmatrix}$$

$$= d(d+2) + 3 = 0$$

$$= d^2 + 2d + 3 = 0 \quad \text{same as char equ.}$$

for continuous time LTI systems, we can write

$$\dot{x} = Ax + Bu$$

$$y = Cx + Du$$

$$x \in \mathbb{R}^n \Rightarrow x = \begin{bmatrix} x_1 \\ x_2 \\ \vdots \\ x_n \end{bmatrix}$$

$$u \in \mathbb{R}^m \Rightarrow \text{control input.}$$

$$y \in \mathbb{R}^p \Rightarrow \text{output vector.}$$

$$A \in \mathbb{R}^{n \times n} \Rightarrow \text{state matrix}$$

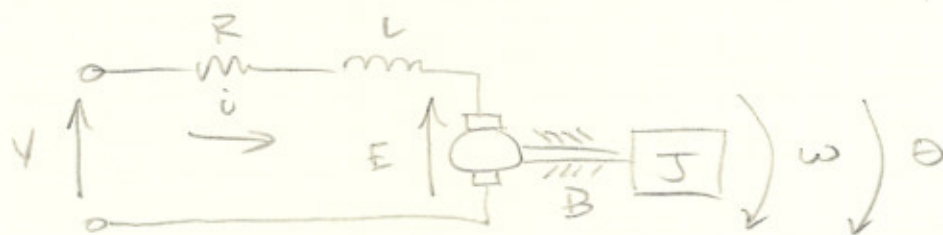
$$B \in \mathbb{R}^{n \times m} \Rightarrow \text{input matrix}$$

$$C \in \mathbb{R}^{p \times n} \Rightarrow \text{output vector.}$$

$$D \in \mathbb{R}^{p \times m} \Rightarrow \text{direct transmission matrix.}$$

note: the only time "D" is different from zero is when the numerator of the transferfunction has an order equal or greater than the denominator.

# DC MOTOR



$$V = Ri + L \frac{di}{dt} + E \quad (1)$$

$$T_m - T_L - B\omega = J\ddot{\theta} \quad (2)$$

$$E = k_1 \omega \quad (3)$$

$$T_m = k_2 i \quad (4)$$

$$\omega = \frac{d\theta}{dt} \quad (5)$$

$$(1) \Rightarrow \frac{di}{dt} = -\frac{R}{L} i - \frac{k_1}{L} \omega + \frac{V}{L}$$

$$(2) \Rightarrow \frac{d\omega}{dt} = -\frac{B}{J} \omega + \frac{k_2}{J} i - \frac{T_L}{J}$$

$$(3) \Rightarrow \frac{d\theta}{dt} = \omega$$

$$x = \begin{bmatrix} i \\ \omega \\ \theta \end{bmatrix} \quad \left. \vphantom{\begin{bmatrix} i \\ \omega \\ \theta \end{bmatrix}} \right\} \text{state vector.}$$

$T_L$ : disturbance,  $\therefore$  let it be zero.  
 $u = V$

$$\dot{x} = Ax + Bu$$

$$A = \begin{bmatrix} -\frac{R}{L} & -\frac{K_t}{L} & 0 \\ \frac{K_t}{J} & -\frac{B}{J} & 0 \\ 0 & 1 & 0 \end{bmatrix} \quad B = \begin{bmatrix} \frac{1}{L} \\ 0 \\ 0 \end{bmatrix}$$

for position control.

$$y = \theta = Cx$$

$$C = [0 \ 0 \ 1]$$

for control of  $\theta, \omega$ .

$$y = \begin{bmatrix} \omega \\ \theta \end{bmatrix} = Cx$$

$$C = \begin{bmatrix} 0 & 1 & 0 \\ 0 & 0 & 1 \end{bmatrix}$$